

Durability assessment of reinforced concrete structures due to chloride ingress up and beyond induction period

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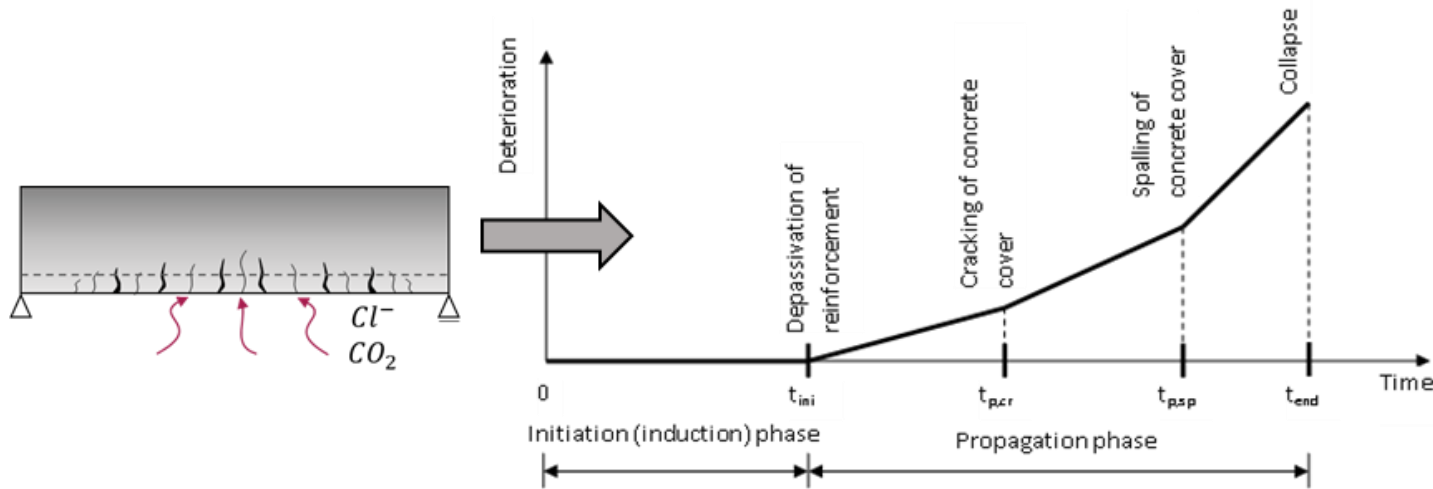
Libor Jendele, Jan Červenka
Červenka Consulting, Ltd.



Outline

- Corrosion of reinforcing steel due to Cl⁻
- Models for induction and propagation phases
- Chemo-mechanical linking
- Examples
 - Bridge strut
 - RC beam from Nougawa bridge

Reinforcing steel corrosion in chloride environment



- Initiation (induction) phase ends when Cl exceeds critical concentration
- Cracks accelerate penetration (0.3 mm crack decreases induction time approximately 5 times)
- Propagation phase forms expanding corrosion products

Model for propagation phase (1)

- 1D chloride concentration (Kwon et al., 2009)

$$C(x,t) = C_s \left[1 - \operatorname{erf} \left(\frac{x}{2\sqrt{D_m(t)f(w)t}} \right) \right] \quad f(w) = 31.61w^2 + 4.73w + 1$$

- Corrosion current density (Liu and Weyers, 1998)

$$i_{corr} = 0.926 \cdot \exp \left[7.98 + 0.7771 \ln(1.69C_t) - \frac{3006}{T} - 0.000116R_c + 2.24t^{-0.215} \right]$$

- 1D model for corrosion depth ($R_{corr} \sim 3$ for pitting)

$$x_{corr}(t) = \int_{t_{ini}}^t 0.0116 i_{corr}(t) R_{corr} dt$$

- Effective bar diameter

$$d(t) = d_{ini} - \psi 2x_{corr}(t)$$

Model for propagation phase (2)

- Cracking of concrete cover (DuraCrete, 2000)

$$x_{corr,cr} = a_1 + a_2 \frac{cover}{d_{ini}} + a_3 f_{t,ch}$$

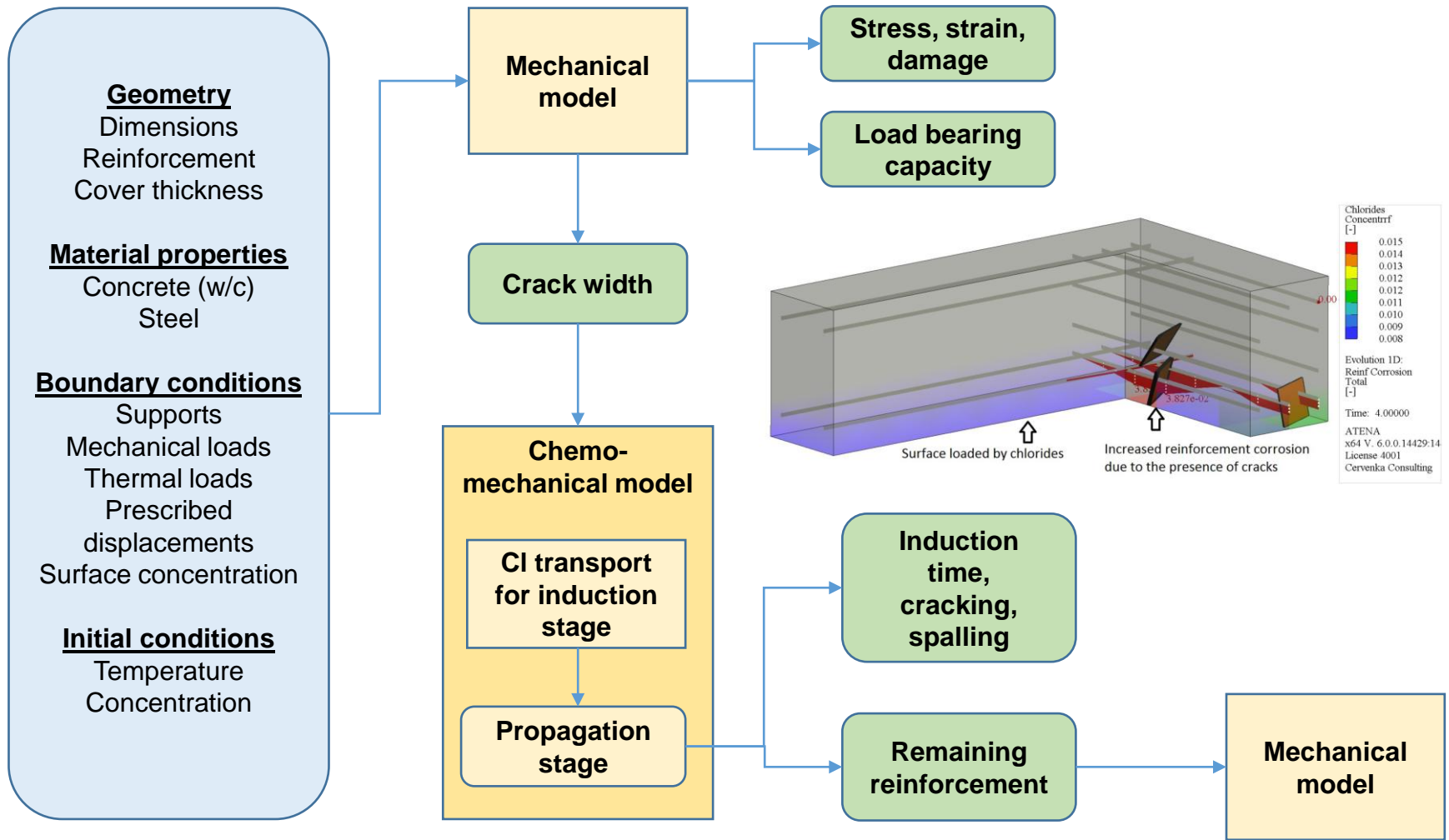
- Spalling of concrete cover (DuraCrete, 2000)

$$x_{corr,sp} = \frac{w^d - w_0}{b} + x_{corr,cr}$$

- Direct steel exposure

Corrosivity zone (ISO 9223)		Typical environment	Corrosion rate for first year (µm/y)	
Category	Description		Mild steel	Zinc
C1	Very low	Dry indoors	≤1,3	≤0,1
C2	Low	Arid/Urban inland	>1,3 a ≤25	>0,1 a ≤0,7
C3	Medium	Coastal and industrial	>25 a ≤50	>0,7 a ≤2,1
C4	High	Calm sea-shore	>50 a ≤80	>2,1 a ≤4,2
C5	Very High	Surf sea-shore	>80 a ≤200	>4,2 a ≤8,4
CX	Extreme	Ocean/Off-shore	>200 a ≤700	>8,4 a ≤25

Simulation workflow

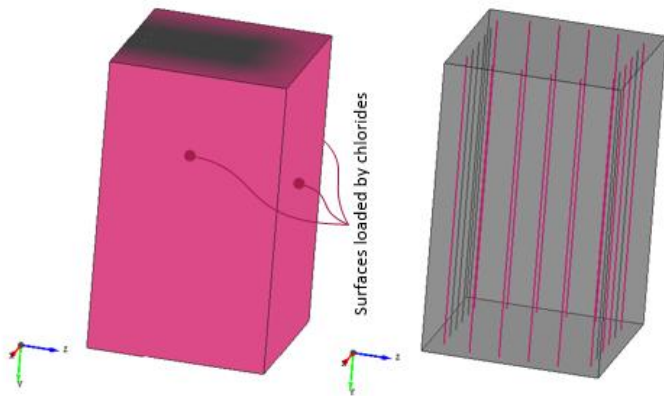


Example 1 – concrete strut

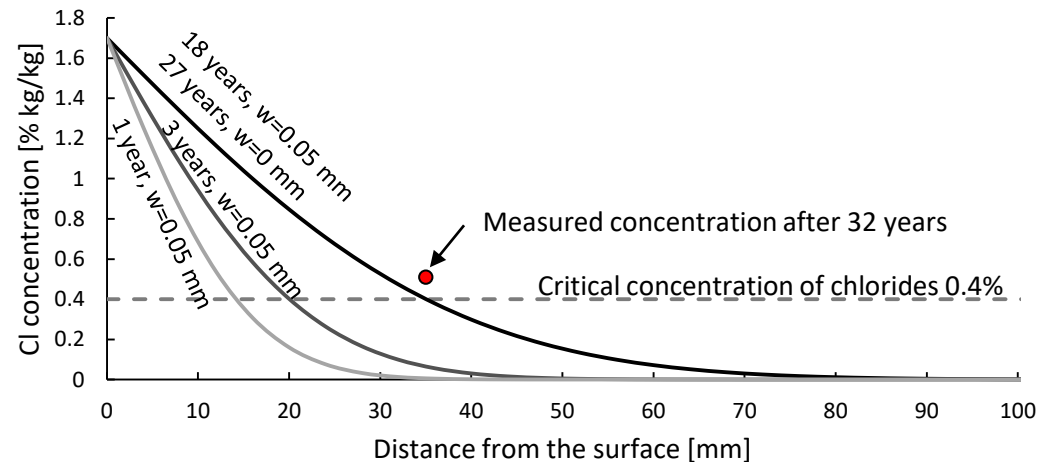
- Prestressed bridge in Prague, 14+36+14 m
- Built 1984, diagnostics 2016
- Struts C35/45 (CEM I 350 kg/m³)
- Bars $\varnothing 32$ mm with stirrups
- Bars' cover 35 mm



[Ing. Junek, Pontex]

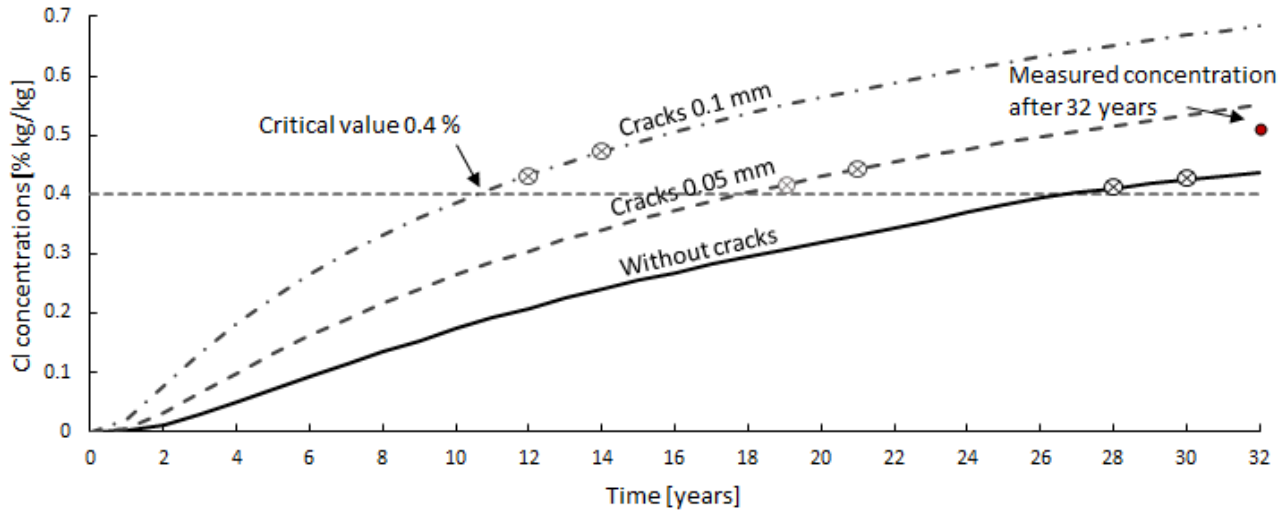


Geometry (0.6 x 0.6 m) of the bridge strut and chloride profile

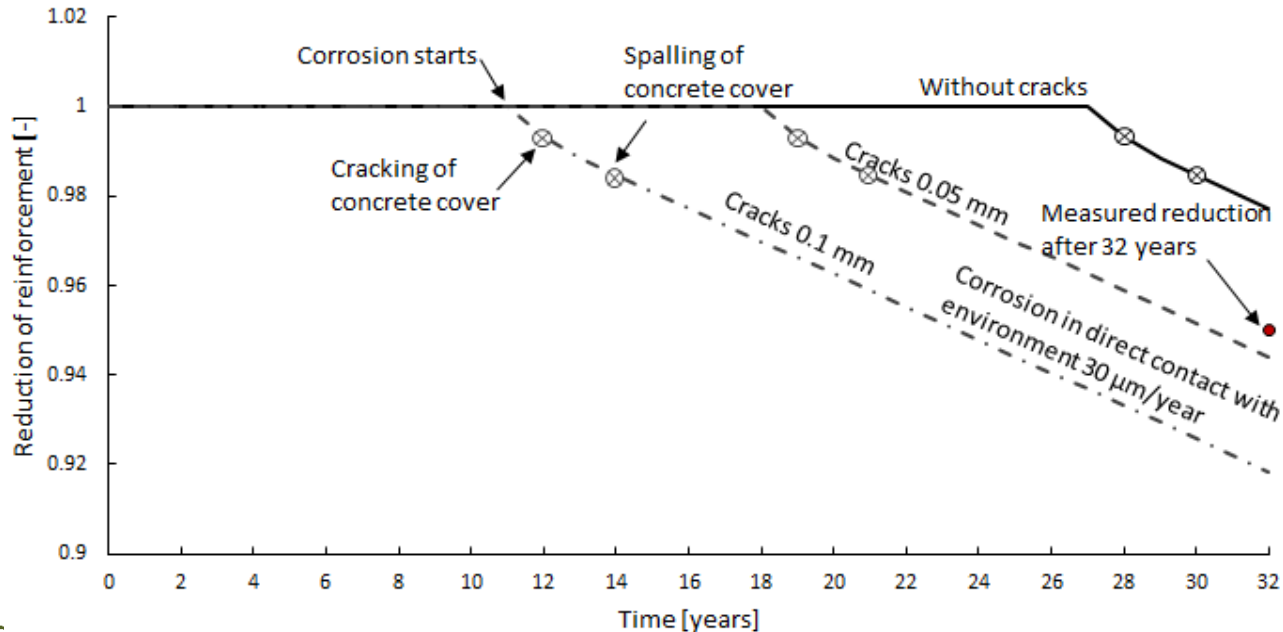


Chloride distribution in the depth of the bridge strut for the surface concentration of 1.7 % kg/kg, induction phase.

Example 1 – concrete strut



Chloride concentrations at the reinforcement depth, concrete cover = 35 mm for three scenarios of crack width.



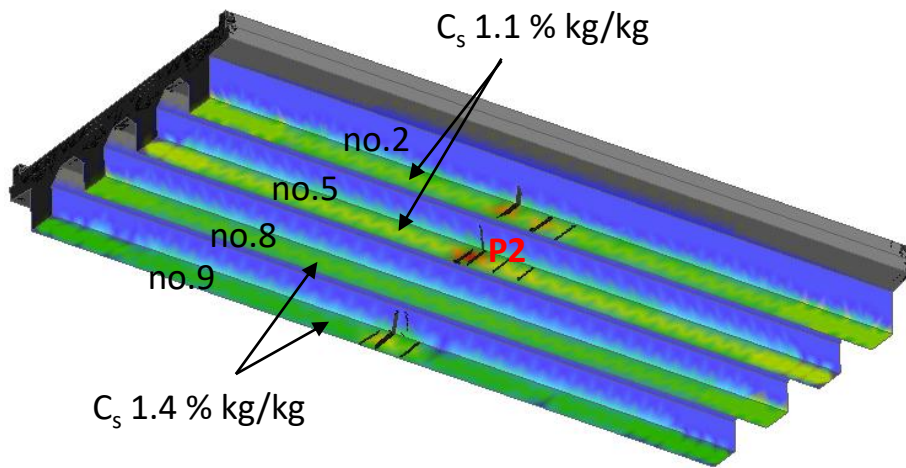
Reduction of the reinforcement area during service life.

Example 2 – Nougawa bridge, Japan

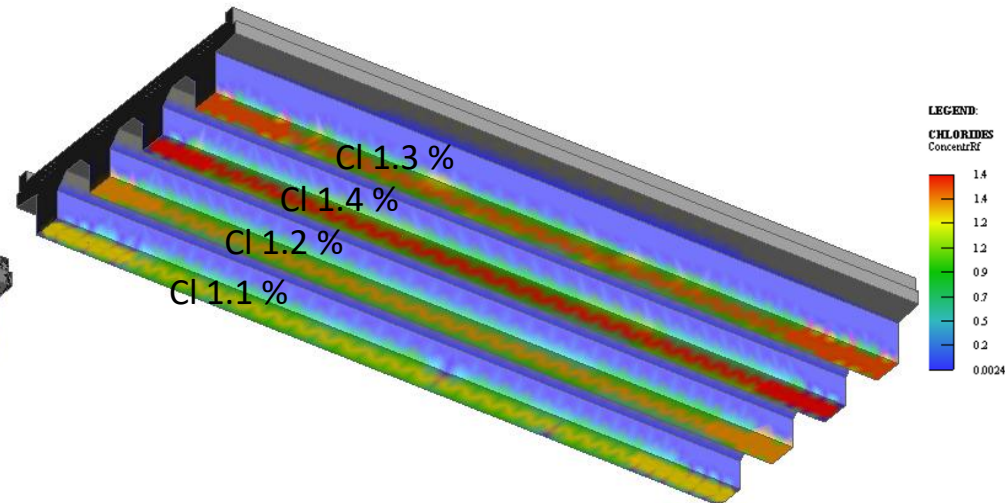
- Built 1930 in coastal area, stirrup's concrete cover 47 mm
- Reinforced beams, 3x4 spans @ 10.8 m = 131 m
- Bars $\varnothing 25.4$ mm, stirrups $\varnothing 9.5$ mm
- Cover restored in 1960, $C_{crit}=0.4\%$
- Two beams tested in 2009



Validated specimen, (Tanaka et al.)



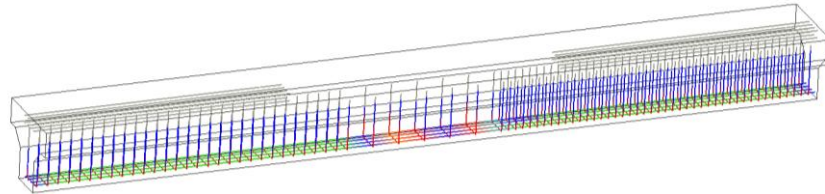
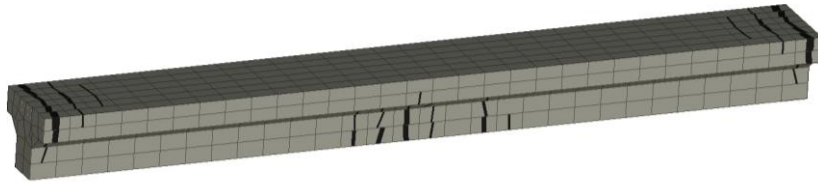
Cl concentration after 30 year in 1960 at 47 mm



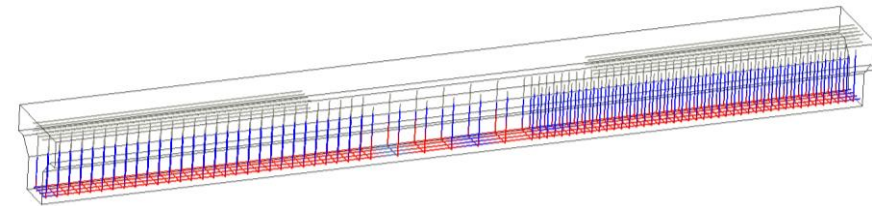
Cl concentration after 80 year in 2010 at 47 mm

Example 2 – Nougawa bridge, Japan

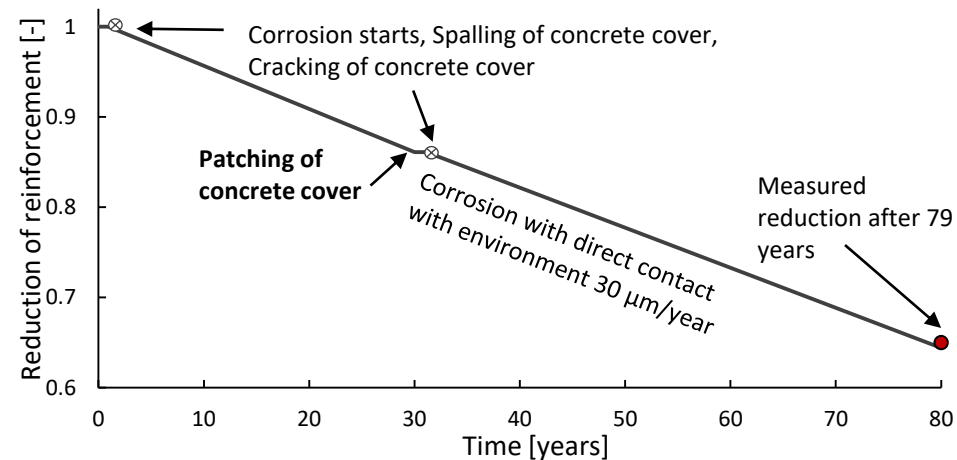
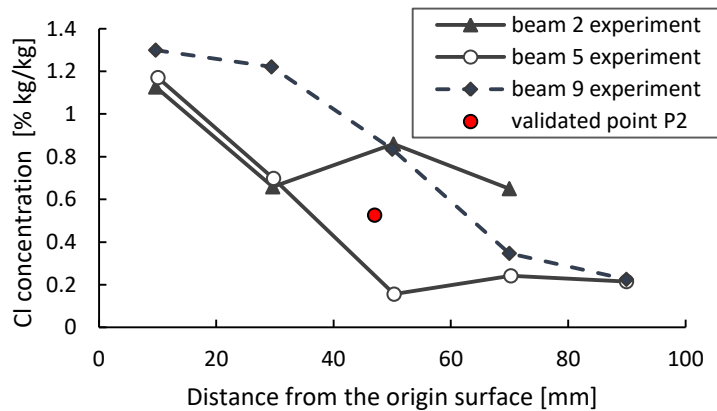
- Predicted reinforcement area of 64% agrees well with the measured value of 62.5%



Reinforcement corrosion after 30 years in 1960

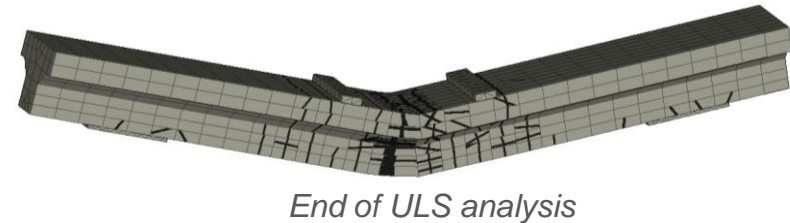
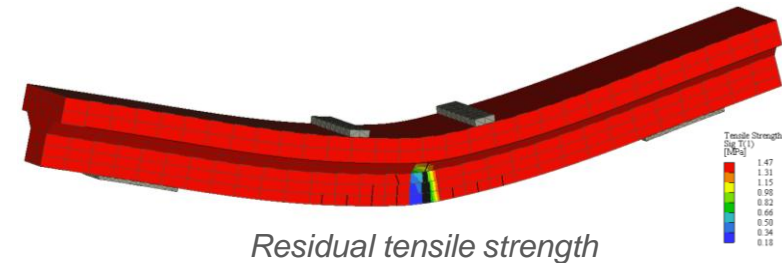
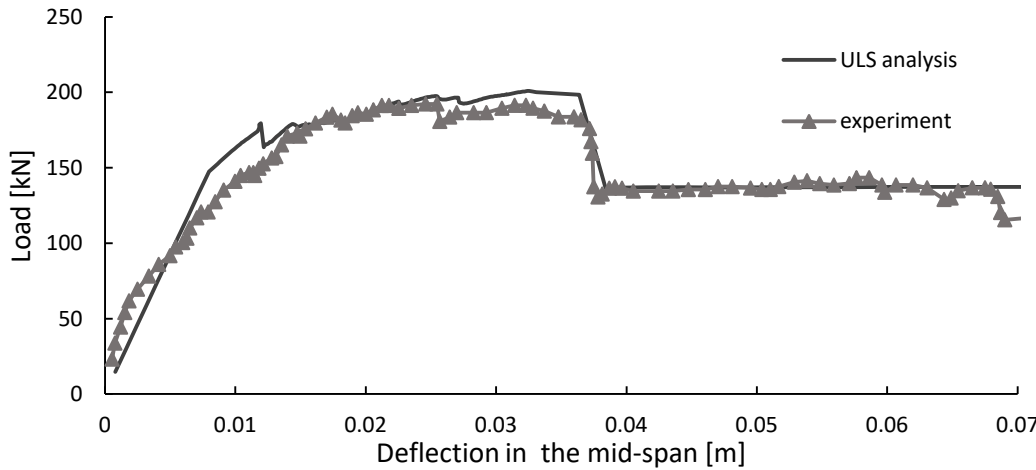
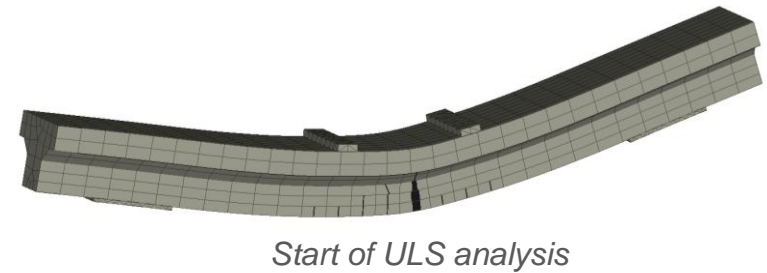
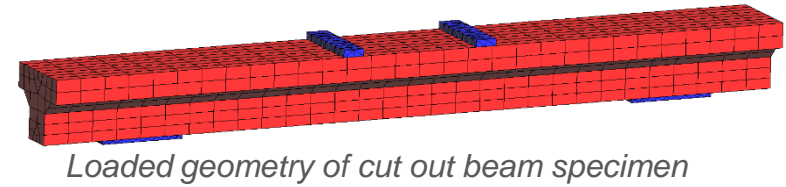
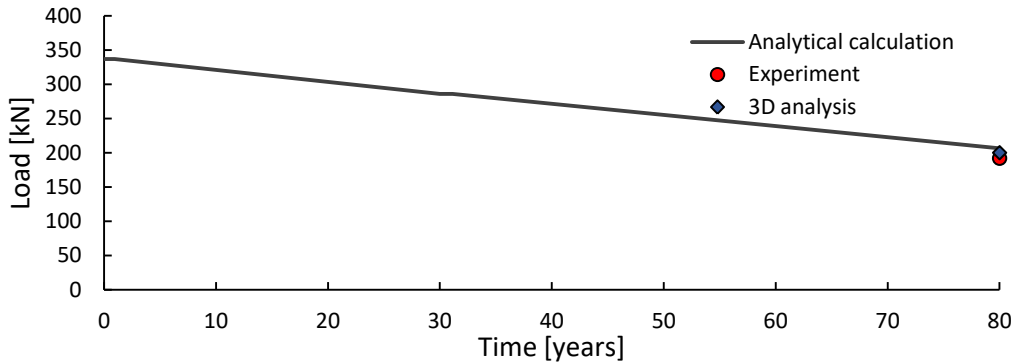


Reinforcement corrosion after 79 years in 2009



Example 2 – Nougawa bridge, Japan

- ULS analysis, 4 point bending @ 3+2+3 m



Conclusions

- Simplified simulation of chloride ingress for reinforced concrete
 - Induction and propagation periods
 - Cl acceleration by crack width
 - Effective reinforcing area
- Further linking with ULS analysis
- Possible linking with LCA

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